# ChE 344 Reaction Engineering and Design

Lecture 3: Thursday, Jan 13, 2022

Rate Laws

Reading for today's Lecture: Chapter 3

Reading for Lecture 4: Chapter 4.1, 4.2

#### Lecture 3: Introduction to Rate Laws Related Text: Chapter 3

**Space time:** 
$$\frac{V}{v_0} = \tau$$
; Space velocity =  $\frac{1}{\tau}$ 

Reaction orders (overall reaction order determines units of rate constant)

$$-r_A = kC_A^{\alpha}C_B^{\beta}; n = \alpha + \beta$$

#### Elementary Rate Laws

Powers in the rate law agree with magnitude of stoichiometric coefficient of the reaction as written.

$$aA + bB \rightarrow C; \frac{-r_A}{a} = kC_A^a C_B^b$$

#### Relative rates (true even if the reaction is not elementary)

$$aA + bB \rightarrow cC + dD$$

$$\frac{r_j}{v_i} = r; r = \frac{r_A}{-a} = \frac{r_B}{-b} = \frac{r_C}{c} = \frac{r_D}{d}$$

 $v_j$  is the stoichiometric coefficient of species j. It is positive if j is a product, and negative if j is a reactant. For example, if the reaction is elementary 'as written' above:

$$r = \frac{-r_A}{a} = \frac{-r_B}{b} = \frac{r_C}{c} = \frac{r_D}{d} = kC_A^a C_B^b$$

#### Temperature dependence of rate constant (Arrhenius equation)

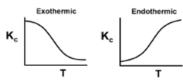
$$k(T) = A \exp\left(-\frac{E_a}{RT}\right)$$
 or  $k(T) = k(T_1) \exp\left(\frac{E_a}{R}\left(\frac{1}{T_1} - \frac{1}{T}\right)\right)$ 

Arrhenius plot:  $ln(k) = ln(A) - \frac{E_a}{R} \frac{1}{T}$ 

#### Temperature dependence of concentration equilibrium constant

$$K_C(T) = K_C(T_1) \exp\left[-\frac{\Delta H_{rxn}}{R}\left(\frac{1}{T} - \frac{1}{T_1}\right)\right]$$

Equilibrium constant can tell you whether a reaction is irreversible  $(\rightarrow)$  or reversible  $(\rightleftarrows)$ .



### Where do rate laws come from? (not covered in Lecture 3)

Collision theory: Frequency of collisions qualitatively gives you the frequency factor/pre-exponential factor for Arrhenius equation, and the concentration dependence (reaction orders).

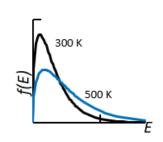
Maxwell-Boltzmann distribution gives you the probability of a collision having a certain energy.

$$f(E,T)dE = \frac{2\pi}{(\pi RT)^{3/2}} \exp\left[\frac{-E}{RT}\right] E^{1/2} dE$$

The integral of the probability gives you the fraction of collisions with energy above some threshold energy  $(E_0)$ .

$$F(E > E_a, T) = \int_{E_a}^{\infty} f(E, T) dE = \frac{2}{\sqrt{\pi}} 2 \left(\frac{E_a}{RT}\right)^{1/2} \exp\left[\frac{-E_a}{RT}\right]$$

The  $\exp\left[\frac{-E_a}{RT}\right]$  is where the exponential portion in the Arrhenius equation comes from! At higher temperatures, a higher fraction of molecular collisions have higher kinetic energies.



From Lecture 2: Design equation for a PBR using conversion. How large does my PBR need to be to reach 80% conversion? Same as PFR, just swap catalyst weight (W) for reactor volume and  $r_A$  for  $r_A$ 

$$-r_A' = F_{A0} \frac{dX}{dW}$$

$$W_{PBR} = F_{A0} \int_0^X \frac{dX}{-r_A'}$$

$$v_0$$
 $C_{A0}$ 
 $F_{A0} = v_0 C_{A0}$ 
 $v$ 
 $C_A$ 
 $F_A = v C_A$ 

Catalyst pellets

Last time: Generalized Mole Balance Equation in Conversion  $X \equiv \text{moles A reacted / moles A fed}$ 

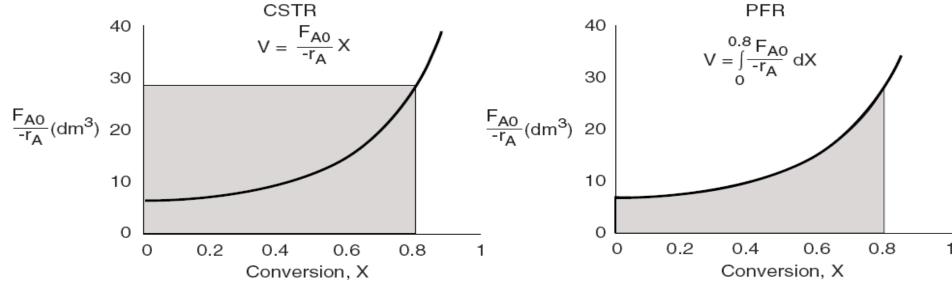
Reactor Differential Algebraic Integral Batch 
$$N_{A0} \frac{dX}{dt} = -r_A V$$
 
$$t = N_{A0} \int_0^X \frac{dX}{-r_A V}$$

CSTR 
$$V_{CSTR} = \frac{r_{A0}X}{-r_A}$$
 
$$PFR F_{A0} \frac{dX}{dV} = -r_A V_{PFR} = F_{A0} \int_0^X \frac{dX}{-r_A}$$

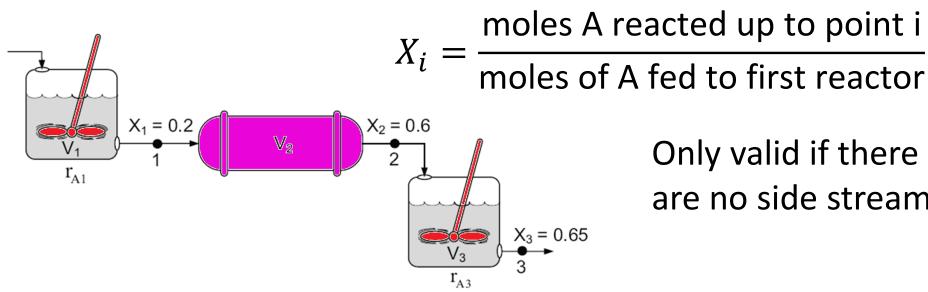
**CSTR** 

PBR 
$$-r_A' = F_{A0} \frac{dX}{dW}$$
 
$$W_{PBR} = F_{A0} \int_0^X \frac{dX}{-r_A'}$$

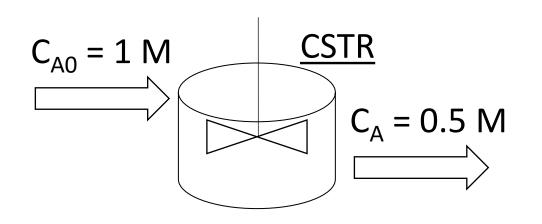
## Last time, Levenspiel plots



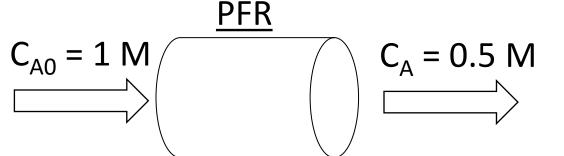
Levenspiel plots can also be used for reactors in series



Only valid if there are no side streams Conceptually: Why different volumes for the same X in a CSTR vs. PFR? Let's look at the reactor concentration for a simple reaction where we want to X = 0.5:  $A \rightarrow B$ 



Rate in **all** of the reactor calculated at  $C_{\Delta} = 0.5$  M



Rate in the reactor calculated at  $C_A > 0.5 M$  (depending where you are in reactor)

If higher  $C_A$  increases the rate of reaction (positive order) the rate will be overall higher in a PFR! Less volume needed

Sometimes rather than volume we will use "space time" in flow reactors: Time to process one reactor volume of fluid For liquid phase:

 $A \rightarrow B$ 

Say CSTR:

$$V_{CSTR} = \frac{F_{j0} - F_j}{-r_j}$$

In liquid phase there is no expansion due to change in number of moles so  $v=v_0$ .

$$\frac{F_{A0}X}{kC_{A0}(1-X)} = \frac{Xv_0}{k(1-X)}$$

Can get (for liquid phase CSTR):

$$\underbrace{\left(\frac{V_{CSTR}}{v_0}\right)}_{} = \frac{X}{k(1-X)}$$

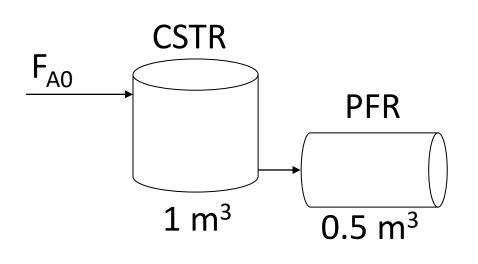
Here spacetime is how long to replace one volume of CSTR. For a PFR it is how long a 'plug' takes to go through a PFR

(defined same way 
$$\frac{V_{PFR}}{v_0}$$
).

$$\frac{1}{\tau} = space \ velocity$$

Sometimes called LHSV, liquid hourly space velocity, while GHSV is the gas hourly space velocity.

Example problem: CSTR and PFR in series (order matters!)



$$F_{A0} = 1 \text{ mol/min}$$
  
 $v_0 = 1 \text{ m}^3/\text{min}$   
 $C_{A0}v_0 = F_{A0}$   
 $A \rightarrow B$ , 1st order in A  
 $k = 1 \text{ min}^{-1}$ 

$$V_{CSTR} = \frac{F_{A0}(X_{out} - X_{in})}{-r_A} = \frac{F_{A0}(X_{out} - X_{in})}{kC_{A0}(1 - X_{out})} = \frac{v_0(X_{out} - X_{in})}{k(1 - X_{out})}$$

$$kV_{CSTR} = v_0(X_{out} - X_{in}) + kX_{out}V_{CSTR}$$
$$kV_{CSTR} + v_0X_{in} = (v_0 + kV_{CSTR})X_{out}$$

$$\frac{kV_{CSTR} + v_0 X_{in}}{v_0 + kV_{CSTR}} = X_{out}$$

$$\frac{1(1) + 1(0)}{1 + 1(1)} = 0.5 = X_{out}$$

Could solve second reactor as a fresh reactor (new  $F_{AO}$ ,  $F_{BO}$ , reset X to 0, then solve), or could continue (but don't mix and match!)

$$V_{PFR} = \int_{X_{in}}^{X_{out}} \frac{-F_{A0}}{r_A} dX = \int_{X_{in}}^{X_{out}} \frac{v_0}{k (1 - X)} dX$$

$$= \int_{X_{in}}^{X_{out}} \frac{1}{(1 - X)} dX = -\ln(1 - X_{out}) + \ln(1 - X_{in})$$

$$X_{out} = 1 - \exp\left[\ln(1 - X_{in}) - k\frac{V_{PFR}}{v_0}\right]$$

Today: Continuing in our Chemical Reacting Engineering algorithm with Rate Laws

Remember they show us the shape of Levenspiel plots!

Ch.5 Lecture 6-7
Ch.4 Lecture 4-5
Ch.3 Lecture 3
Ch.1 Lecture 1

Heat Effects

Isothermal Design
Stoichiometry

Rate Laws

Mole Balance

Why are rate laws important?

We need  $r_A = f(X)$  to be able to determine reactor sizes needed to reach a certain conversion.

$$-r_A = [k(T)][f(C_A, C_B...)]$$

Recall that k is our rate 'constant' (but actually a function of temperature as we will learn today)

$$C_i = f(X)$$

As your reaction proceeds (conversion increases), naturally the concentrations will change! A rate law allows you to understand how this change influences your rate

## For a generic reaction

$$aA + bB \rightleftharpoons cC + dD$$

## Power law

$$-\frac{r_A}{a} = kC_A^{\alpha}C_B^{\beta}$$

 $\alpha$  is reaction order in A

**B** is reaction order in B

Overall order is  $n = \alpha + \beta$ 

# Elementary rate law

The powers in the rate law agree with the magnitude of the stoichiometric coefficient (i.e.,  $\alpha$  = a,  $\beta$  = b)

Example: 
$$1A + 2B \rightarrow C$$

Example: 
$$1A + 2B \rightarrow C$$

$$-r_A = kC_A^1 C_B^2 = kC_A C_B^2$$

We would say A is first order and B is second order C is zero order

Many reactions are non-elementary and may have complex relations with concentrations

(Just a simplified example, we won't derive until we discuss catalysis later in the course)

$$-r_A = k \frac{C_A C_B}{(1 + C_A + C_B)^2}$$

If 
$$C_A \gg C_B + 1$$

$$-r_A \approx k \frac{C_A C_B}{(C_A)^2}$$

$$-r_A \approx k(C_A)^{-1}C_B$$

If  $C_A \ll C_B + 1$ 

$$-r_A \approx k \frac{C_A C_B}{(1 + C_B)^2}$$

$$-r_A \approx kC_A \frac{C_B}{(1+C_B)^2}$$

Negative one order in A when  $C_A$  is high!

Positive one order in A when  $C_A$  is low!

Units of rate constant *k* are determined by order of reaction!

Recall: reaction rate has units mol/(volume\*time)

Concentration has units of mol/volume

## Zero order overall

$$-r_A = k$$

k has units of mol/(volume\*time)

## First order overall

$$-r_A = kC_A^1$$

k has units of (time<sup>-1</sup>)

# Second order overall

$$-r_A = kC_A^1 C_B^1$$
$$-r_A = kC_A^2$$

k has units of volume/(mol\*time)

# Discuss with your neighbors:

You are running the following reaction in a flow reactor, and when you decrease  $C_A$  (without changing anything else), your amount of B produced per hour goes down. Which of the following *cannot* be the rate law?

$$A \rightarrow B$$

A) 
$$r_A = -kC_A$$
 Elementary

B) 
$$r_A = -k$$

Positive non-zero order only

C) 
$$r_A = -k(C_A)^{3/2}$$

$$\mathsf{D}) \qquad \mathsf{r}_{\scriptscriptstyle \Delta} = -\mathsf{k}(\mathsf{C}_{\scriptscriptstyle \Delta})^{1/2}$$

 $r_j = v_j r$  where r is the rate of reaction Stoichiometric coefficient of j

$$\frac{-r_A}{a} = \frac{-r_B}{b} = \frac{r_C}{c} = \frac{r_D}{d}$$

Example: Elementary rate law  $A + 2B \rightarrow 4C$ 

$$\frac{-r_A}{1} = \frac{-r_B}{2} = \frac{r_C}{4}$$

In the book, Prof Fogler uses rate constants with a subscript

$$-r_A = k_A C_A C_B^2$$
;  $-r_B = k_B C_A C_B^2$ ;  $r_C = k_C C_A C_B^2 = 4k_A C_A C_B^2$ 

In lecture slides I will use a single rate constant relative to the written reaction.

$$r_A = \nu_A k C_A C_B^2 = -k C_A C_B^2$$

$$r_B = \nu_B k C_A C_B^2 = -2k C_A C_B^2$$

$$r_C = \nu_C k C_A C_B^2 = 4k C_A C_B^2$$

How about moving from irreversible to reversible reactions?

$$k_{\text{forward}} = k_f$$

$$2A + B \rightleftarrows 3C$$

$$k_{\text{reverse}} = k_r$$

If elementary rate law:

$$\frac{r_A}{-2} = \frac{r_B}{-1} = \frac{r_C}{3} = k_f C_A^2 C_B - k_r C_C^3 = k_f \left[ C_A^2 C_B - \frac{C_C^3}{k_f / k_r} \right]$$

$$= k_f \left[ C_A^2 C_B - \frac{C_C^3}{K_C} \right]$$

$$= k_f \left[ C_A^2 C_B - \frac{C_C^3}{K_C} \right]$$
Conc. equilibrium constant If elementary!

If  $K_C$  is very large,  $k_f \gg k_r$ , and the reaction can be assumed to be irreversible!

From thermodynamics:

Equilib.

concentrations

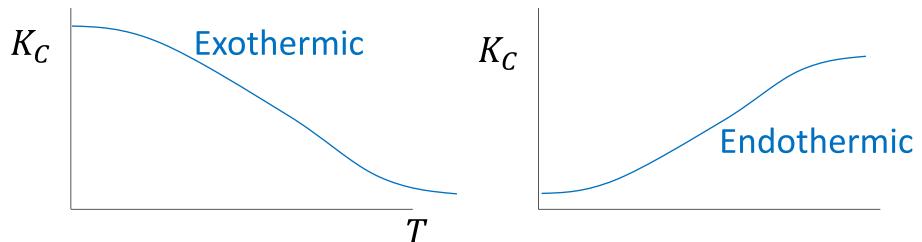
$$K_C = \prod_i C_{i,eq}^{\nu_i} = \frac{C_{C,eq}^3}{C_{A,eq}^2 C_{B,eq}}$$

If  $K_C$  is very large,  $C_{B,eq}$  and  $C_{A,eq}$  approach zero (X  $\rightarrow$  1)

$$K_C(T) = K_C(T_1) \exp \left[ -\frac{\Delta H_{rxn}}{R} \left( \frac{1}{T} - \frac{1}{T_1} \right) \right]$$

An exothermic reaction has a  $\Delta H_{rxn}$  that is negative.

An endothermic reaction has a  $\Delta H_{rxn}$  that is positive.



T

$$K_C = \frac{C_{C,eq}^3}{C_{A,eq}^2 C_{B,eq}}$$

$$-\frac{r_A}{2} = k_f \left[ C_A^2 C_B - \frac{C_C^3}{K_C} \right] = k_f C_A^2 C_B - k_r C_C^3$$

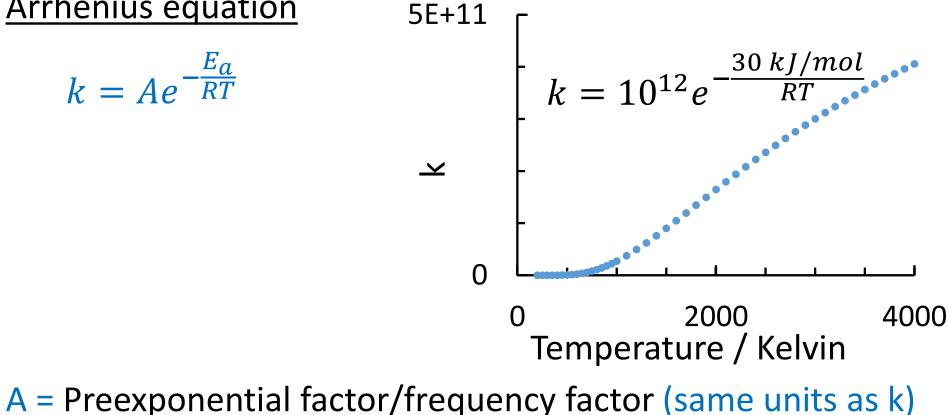
At equilibrium, no reaction:  $r_A = 0$ 

$$C_{A,eq}^2 C_{B,eq} = \frac{C_{C,eq}^3}{K_C}$$

$$K_C = \frac{C_{C,eq}^3}{C_{A,eq}^2 C_{B,eq}}$$

Same for an elementary reaction!

Reaction rates depend on temperature through rate constant Arrhenius equation 5E+11



R = ideal gas constant, 8.314 J mol<sup>-1</sup> K<sup>-1</sup>  $E_a$  = activation energy, units J mol<sup>-1</sup> (or kJ/mol)

T in Kelvin (important it is in absolute temp!)

Often, you will have information about k at a given temperature, but need to know it at a different temperature.

For k that is known at a given temperature  $T_1$ 

$$k(T_1) = A \exp\left(-\frac{E_a}{RT_1}\right)$$

You can solve for *k* at a temperature T

$$k(T) = A \exp\left(-\frac{E_a}{RT}\right)$$

$$\frac{k(T)}{k(T_1)} = \frac{A}{A} \frac{\exp\left(-\frac{E_a}{RT}\right)}{\exp\left(-\frac{E_a}{RT_1}\right)} = \exp\left(\frac{E_a}{R}\left(\frac{1}{T_1} - \frac{1}{T}\right)\right)$$

$$k(T) = k(T_1) \exp\left(\frac{E_a}{R} \left(\frac{1}{T_1} - \frac{1}{T}\right)\right)$$

 $E_a$  is essentially always positive. With this in mind...

# **Discuss with your neighbors:**

The rate constant, k, at 300 Kelvin is 1 s<sup>-1</sup>. The activation energy,  $E_a$ , is 99.6 kJ/mol. What is k at 350 Kelvin? Hint: You should not need a calculator (but feel free to if you want).

$$k(T) = k(T_1) \exp\left(\frac{E_a}{R} \left(\frac{1}{T_1} - \frac{1}{T}\right)\right)$$
A) 300 s<sup>-1</sup>

B) 300 M<sup>-1</sup> s<sup>-1</sup> Won't change units, positive E<sub>a</sub> means rate constant goes up with temperature

C) 
$$0.1 \, \text{s}^{-1}$$

$$= 1s^{-1} \exp\left(\frac{99.6 \, kJ mol^{-1}}{8.314 \, J \, mol^{-1} K^{-1}}\right)$$

$$*\left(\frac{1}{300\ K}-\frac{1}{350\ K}\right)\right)$$

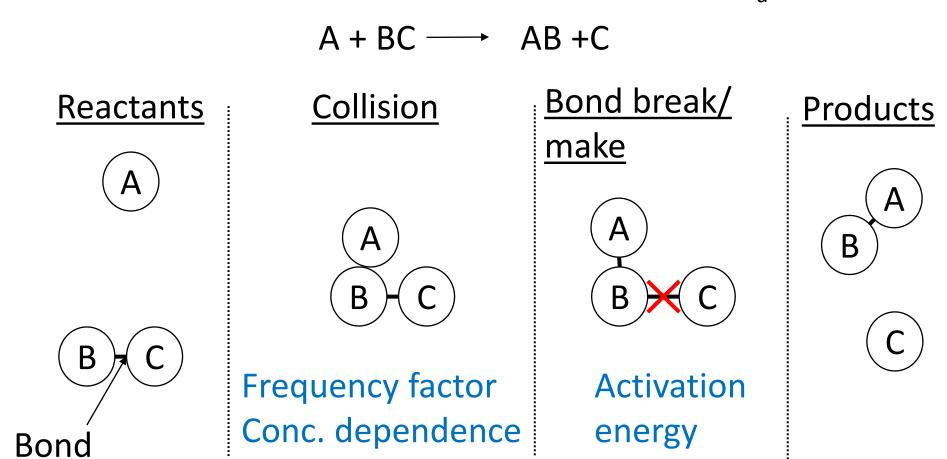
The effective activation barrier can be extracted using an Arrhenius plot

$$k = Ae^{-\frac{E_a}{RT}}$$

$$|n[k]| = \ln[Ae^{-\frac{E_a}{RT}}]$$

$$|n[k]| = \ln[A] - \frac{E_a}{RT}$$

- Why do rate laws have the form we see and why is there an activation energy? One way to think about it.
- Qualitatively it is because the reactants must:
- 1. collide (higher concentration = more chance for collisions)
- 2. break/make new bonds which takes energy (E<sub>a</sub>)!



- The energy to make/break bonds comes from the kinetic energy of the molecules when they collide.
- The distribution of velocities of the reacting molecules relative to one another is given by the Boltzmann distribution.

$$f(U,T) = 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \exp\left[\frac{-mU^2}{2k_B T}\right] U^2$$

 $k_{\rm B}$  = Boltzmann's constant = 1.38 x 10<sup>-23</sup> J/molecule/K m = Reduced mass, g U = Relative velocity, m/s T = Absolute Temperature, K f(U,T) = distribution of relative velocities

f(U,T)dU = fraction of relative velocities from U to U+dU

$$f(U,T) = 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \exp\left[\frac{-mU^2}{2k_B T}\right] U^2$$

e = Kinetic energy per molecule (not mole)

$$e = \frac{1}{2} mU^2$$

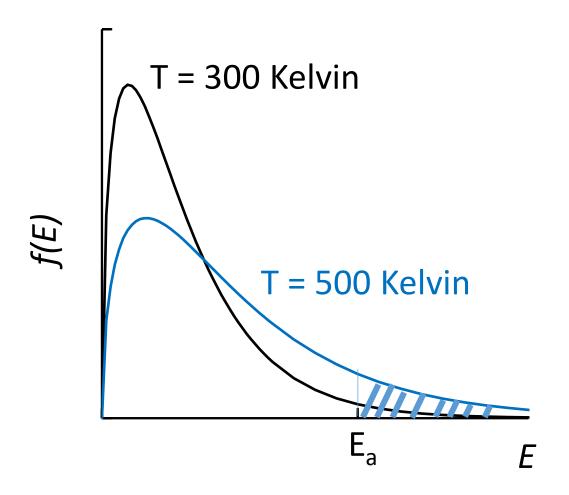
$$f(e,T) = \frac{2\pi}{(\pi k_B T)^{3/2}} \exp\left|\frac{-e}{k_B T}\right| e^{1/2}$$

Switch e (kJ/molecule) to E (kJ/mol), and  $k_B$  to R

$$f(E,T) = \frac{2\pi}{(\pi RT)^{3/2}} \exp\left[\frac{-E}{RT}\right] E^{1/2}$$

$$f(E,T)dE = \frac{2\pi}{(\pi RT)^{3/2}} \exp\left[\frac{-E}{RT}\right] E^{1/2} dE$$

Fraction of collisions with energy E and E + dE



Fraction of molecules with energy  $E > E_a$ 

$$F(E > E_a, T) = \int_{E_a}^{\infty} f(E, T) dE$$

Fraction of collisions with energy greater than E<sub>a</sub>

$$F(E > E_a, T) = \frac{2}{\sqrt{\pi}} 2\left(\frac{E_a}{RT}\right)^{1/2} \exp\left[\frac{-E_a}{RT}\right]$$

Back to Arrhenius equation:

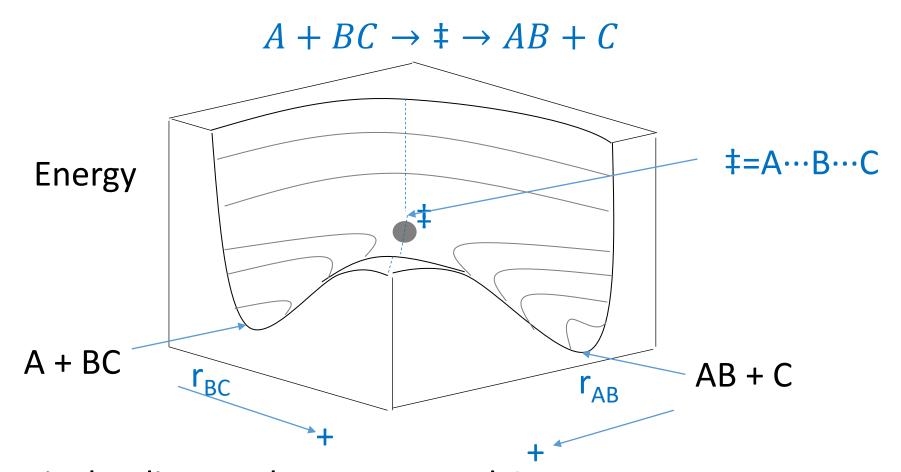
$$k(T) = A \exp\left(-\frac{E_a}{RT}\right)$$
Exaction of our

Collisions, or opportunities to react per time

Fraction of opportunities that result in a reaction

Rate constant will never exceed A, because as  $T \to \infty$ ,  $\exp\left(-\frac{E_a}{PT}\right) \to 1$ 

Another way to explain Arrhenius- Potential Energy Surface: Every configuration has an associated energy.



r<sub>BC</sub> is the distance between B and C

The transition state (‡) is the highest energy position along the lowest energy pathway from reactant to product